Detailed balance limit of silicon nanowire and nanohole array solar cells

Chenxi Lin* and Michelle L. Povinelli
Ming Hsieh Department of Electrical Engineering, University of Southern California, 3651 Watt Way, Los Angeles, CA, USA 90089-0106
*chenxil@usc.edu

ABSTRACT

In this proceeding, we use optical modeling and detailed balance analysis to predict the limiting efficiency of nanostructured silicon solar cells based on vertically-aligned nanowire and nanohole arrays. We first use the scattering matrix method to study broadband optical absorption. By incorporating the calculated optical absorption into a detailed balance analysis, we obtain the limiting short circuit current, open circuit voltage, and power conversion efficiency of nanowire and nanohole solar cells. Results show that optimized nanowire and nanohole arrays of 2.33 microns in height have 83% and 97% higher power conversion efficiencies than a thin film with the same height, respectively. Furthermore, we find that the limiting power conversion efficiency is mainly determined by the short circuit current density, which is proportional to the broadband optical absorption.

Keywords: silicon nanowire array, silicon nanohole array, photonic crystal slab, absorption enhancement, light trapping, guided resonances, detailed balance limit, solar cells.

1. INTRODUCTION

Microstructured broadband absorbers hold great promise for cheaper, more efficient solar cells. Recent work has established that material microstructure can be tailored to achieve large absorption, even within a depth shorter than the optical absorption length. This approach, which we term structural absorption engineering, relies on carefully-designed microstructures to achieve efficient light trapping. Vertically-aligned silicon nanowire and nanohole arrays provide model systems to study structural absorption enhancement. In our previous work, we have shown theoretically that silicon nanowire array with optimized geometrical parameters have a higher broadband absorption than a thin film of the same height. This effect is due to a combination of anti-reflection and light trapping properties, including the excitation of guided resonance modes. Similar conclusions have been found for silicon nanohole arrays. However, previous work calculated the ultimate efficiency of nanowire and nanohole structures, an upper bound on the efficiency that depends on optical absorption alone and does not consider the electrical properties of the cell. In this proceeding, we extend our previous work to calculate a modified detailed balance limit on the efficiency of silicon nanowire and nanohole array solar cells.

The detailed balance limit of a solar cell, also known as the “Shockley-Queisser limit”, is a fundamental physical limit on power conversion efficiency obtained by considering only intrinsic loss mechanisms. The original Shockley-Queisser analysis considered bulk solar cells. The short circuit current is proportional to the total number of photons above the band gap; it is assumed that all such photons are absorbed to generate electron-hole pairs. The value of reverse saturation current density is set by assuming that radiative recombination is the only recombination mechanism, and an ideal diode characteristic is used to describe the electrical properties of the solar cell.

Here we apply a modified detailed balance analysis to nanowire and nanohole geometries. As in Ref.33, we take into account the realistic optical absorption spectrum, rather than assuming perfect absorption above the band gap. In this way, we obtain a practical limiting efficiency for nanostructured thin film solar cells. We show that the detailed balance limit yields an efficiency for both optimized nanowire arrays and optimized nanohole arrays that is higher than a thin film with the same height. The optimal structural parameters for the arrays are similar to those obtained in our previous work, which used optical modeling alone.
2. METHODS

Accurate optical modeling is used to determine an upper limit on solar cell efficiency, assuming perfect carrier collection and modeling the electrical properties of the cell as an ideal diode.

2.1 Optical modeling

Figure 1 shows vertically aligned silicon nanowire (a) and nanohole (b) arrays. Each array consists of a square lattice with lattice constant \( a \). The diameter of the wire or hole is indicated by \( d \). The filling ratio is defined as the fractional area occupied by Si in one unit cell, given by \( \frac{\pi d^2}{4a^2} \) for nanowire arrays and \( 1 - \frac{\pi d^2}{4a^2} \) for nanohole arrays. We study an array thickness \( L \) of 2.33μm, comparable to the thickness of silicon thin film solar cells. The thickness is shorter than the absorption length of crystalline silicon for wavelengths greater than ~600nm. The nanowire and nanohole structures are surrounded by air.

The structures are illuminated at normal incidence, as indicated by the red arrow. The electric field is polarized parallel to the direction between nearest-neighbor rods (or holes). The ASTM Air Mass 1.5 direct and circumsolar solar spectrum is used to model the solar irradiance.

We use a full-vectorial electromagnetic solver to calculate the wavelength-dependent absorptance, \( A(\lambda) \), of the nanowire and nanohole structures. Simulations are performed using the ISU-TMM package, an implementation of the scattering matrix method. The refractive index and absorption coefficient of the silicon regions are set to the experimentally determined, wavelength-dependent values for bulk silicon.

2.2 Modified detailed balance limit

The short circuit current can be related to the absorptance by

\[
J_{sc} = \frac{e}{hc} \lambda_g A(\lambda) \lambda d\lambda 
\]

where \( \lambda_g = 1127 \text{nm} \) is the band gap of silicon, and the solar irradiance is negligible below 310nm. Eq. (1) assumes perfect carrier collection and so represents an upper bound on the short circuit current.

We use the \( J-V \) characteristic of an ideal diode to describe the electrical properties of the solar cell:

\[
V(J) = k_B T \frac{q}{q} \ln \left( \frac{J_{sc} - J}{J_0 A_{junc}} \right) + 1 \approx k_B T \ln \left( \frac{J_{sc} - J}{J_0 \gamma} \right) + 1, \quad \gamma = \frac{A_{junc}}{A_{illu}}
\]

in which \( J \) is the current density of the solar cell, \( V \) is the voltage between the terminals of the cell, and \( J_0 \) is the reverse saturation current density. \( A_{illu} \) is the illumination area, and \( A_{junc} \) is the junction area. In planar thin films, \( \gamma \) equals unity. In nanostructured thin films, \( \gamma \) depends upon the specific junction geometry. Here we assume an axial p-n junction geometry, where the \( p \) and \( n \) regions are vertically stacked. Therefore, \( \gamma \) is equal to the filling ratio of the array.
We take the value of the reverse saturation current density to be [39]:

\[
J_0 = \frac{2\pi a}{h^3 c^2} (n_f^2 + n_B^2) k_B T (2k_B T + 2k_B T \epsilon + E_g^2) \exp(-\frac{E_g}{k_B T})
\]

where \(n_f\) and \(n_B\) are the refractive indices of the superstrate and substrate of the solar cell, equal to 1 (air). For crystalline silicon with a band gap of 1.1eV at \(T = 300K\), the value of \(J_0\) is \(5.4 \times 10^{-13}\) mA/cm².

By setting the total current \(J = 0\), we obtain the open circuit voltage of the solar cell. Under the assumption that \(J_{sc} >> J_0\),

\[
V_{oc} - V(J = 0) = \frac{k_B T}{q} \ln \left( \frac{J_{sc}}{J_0 \gamma} \right) + 1 \approx \frac{k_B T}{q} \ln \left( \frac{J_{sc}}{J_0 \gamma} \right) = \frac{k_B T}{q} \ln \left( \frac{J_{sc}}{J_0} \right) - \frac{k_B T}{q} \ln \gamma
\]

The power conversion efficiency is defined as

\[
P.C.E = \frac{V_{mpp} J_{mpp}}{I_{in}} = \frac{V_{oc} J_{sc} FF}{I_{in}}
\]

where \(V_{mpp}\) and \(J_{mpp}\) are the voltage and current density that maximize the power \(J \times V(J)\), \(FF = V_{mpp} J_{mpp} / V_{oc} J_{sc}\) is the fill factor, and \(I_{in}\) is the incident solar power density. For the ASTM AM1.5 direct and circumsolar solar spectrum, \(I_{in}\) is about 900.14 W/m².

For a given nanowire or nanohole structure, the power conversion efficiency can be determined numerically using Eq. 2 and the value of the short circuit current can be obtained from the optical simulation (Eq. 1).

### 3. RESULTS

Figure 2 shows calculation results for nanowire (a, c, e) and nanohole (b,d,f) arrays. We plot the short circuit current density, open circuit voltage, and power conversion efficiency for arrays with various structural parameters (lattice constant and filling ratio).

Figures 2 (a) and (b) show \(J_{sc}\) as a function of lattice constant and filling ratio for nanowire and nanohole arrays, respectively. In both cases, the maximum values of \(J_{sc}\) are obtained for lattice constants in the 600nm – 700nm range and moderate filling ratio (~0.5). The value of the short circuit current density is higher than that for a thin film with the same thickness. It is also higher than the value for a thin film with a single-layer Si₃N₄ AR coating.

Figures 2 (c) and (d) show \(V_{oc}\) as a function of lattice constant and filling ratio. \(V_{oc}\) increases with decreasing filling ratio for both nanowires and nanoholes. The variation in voltage is small (~6%) over the range of parameters plotted. From Eq. (4), \(V_{oc}\) scales as \(\ln(J_{sc}/\gamma)\), where \(\gamma\) is the filling ratio. \(J_{sc}\) depends on \(\gamma\), as seen above in Figures 2(a) and (b). Thus, the value of the filling ratio that optimizes \(J_{sc}\) does not necessarily optimize \(V_{oc}\). Inspection of Figures 2(a) and 2(c) reveals that this is the case only for nanowire arrays.

We found that the fill factor (Eq. 5) is approximately 86% over the range of lattice constants and filling ratios considered.

Figures 2 (e) and (f) show the power conversion efficiency. The optimal nanowire structure (\(a=650nm\) and \(d=520nm\)) has an efficiency of 15.98%. The optimal nanohole array structure (\(a=600nm\) and \(d=480nm\)) has an efficiency of 17.18%. These values are higher than for a silicon thin film with the same thickness (8.71%), and even for a thin film with an optimal single-layer Si₃N₄ AR coating (12.99%). The dependence of efficiency on lattice constant and filling ratio is very similar to the short circuit current density (Figures 2(a) and (b)), which can be attributed to the much more significant variation in the short circuit current density than the open circuit voltage.
Figure 2 The dependence of solar cell characteristics on lattice constant and filling ratio for nanowire (a, c, e) and nanohole (b, d, f) arrays.
4. CONCLUSION AND DISCUSSION

To summarize, we have calculated an upper bound on the power conversion efficiency of silicon nanowire and nanohole solar cells. Our approach uses rigorous optical modeling in combination with a diode model of the current-voltage characteristics and assumes perfect carrier collection. The results show that both silicon nanowire and nanohole arrays with optimized structural parameters outperform an AR-coated thin film of the same thickness. Nanowire and nanohole arrays exhibit higher short circuit current, open circuit voltage, and power conversion efficiency. The dependence of the power conversion efficiency on the structural parameters of the arrays (filling ratio and lattice constant) largely follows that of the short circuit current, which is proportional to the broadband optical absorption.

We have assumed an axial p-n junction geometry in our analysis. Another possible geometry is the radial p-n junction\(^{39}\). We have calculated the power conversion efficiency of radial junction geometries, and the values are generally lower. This is due to the increase in junction area, corresponding to \(\gamma > 1\) in Eq. (4), which leads to a decrease in the open circuit voltage.

Further work may incorporate more detailed and realistic models of the electro-optical properties of the cell. Above, we have assumed a constant value of the reverse saturation current density, \(J_0\) (Eq. 3). Due to the possibility of emission enhancement in nanostructured films\(^{33}\), \(J_0\) may vary with the filling ratio and lattice constant of nanowire or nanohole arrays. Moreover, we have assumed perfect carrier collection. It should be possible to place a stricter bound on power conversion efficiency using detailed device physics models\(^{39,40}\).

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